STABILITY OF LOCALIZED MHD MODES IN DIVERTOR TOKAMAKS – A PICTURE OF THE H-MODE

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ABSTRACT. The paper examines the stability of a model divertor tokamak equilibrium to MHD ballooning and interchange modes. The combined effects of the magnetic separatrix and a finite edge current density can result in coalescence of the first and second stable regions. This leads to a picture of the H-mode in which the observed steep edge pressure gradients result from the modified ballooning stability properties.

1. INTRODUCTION

Application of neutral injection heating to tokamak plasmas generally results in a degradation of energy confinement. However, tokamaks with poloidal divertors may exhibit an improved confinement regime, the H-mode, in which the confinement time is comparable to that observed with Ohmic heating [1–3]. In such experiments the boundary of the plasma is defined by a magnetic separatrix. An outstanding feature of the H-mode is the occurrence just inside the separatrix of very steep gradients of density and temperature, and therefore of pressure. Since pressure gradients can be limited by the onset of ballooning and interchange modes, it is of interest to examine how the stability properties of such modes are modified by the presence of the separatrix.

Recently the experimental pressure profiles have been examined (on ASDEX) for their stability to ideal ballooning modes [4]. The theoretical criterion used, however, was the $s$-$\alpha$ model [5] which describes circular flux surfaces with constant poloidal field and which therefore neglects the presence of the separatrix and its effects on MHD stability. In a previous paper on ballooning stability in the vicinity of a separatrix [6] a model equilibrium was introduced to describe the plasma in a divertor tokamak. (This equilibrium represents a generalization of the $s$-$\alpha$ model.) The present work extends the work presented in Ref. [6] to allow for finite current density. We use a slightly modified equilibrium model and ballooning equation, and for completeness we give a brief résumé of the equilibrium in Section 2. We then examine the modified ballooning stability properties at zero current density. The stability of ballooning modes on the separatrix itself has been considered by Qu and Callan [7]. The effects of flux surface shaping on the first stability boundary have been discussed by Pogutse et al. [8].

In Section 3 we consider the stability of localized ideal interchange modes and comment on the close connection between these and the ballooning modes. The Appendix deals with the stability of resistive interchange modes.

The effects on stability of a non-zero current density are investigated in Section 4. A non-zero current density can result in the coalescence of the first and second stable regions for flux surfaces sufficiently close to the separatrix. The plasma in this region is then stable for any value of the pressure gradient. A possible explanation for this effect is given in Section 5. These results lead in Section 6 to an interpretation of the H-mode in terms of ideal MHD stability properties. Quantitative predictions of the model are found to be in broad agreement with experimental results. Conclusions are drawn in Section 7.

2. MODEL EQUILIBRIUM AND BALLOONING STABILITY

We begin with a brief review of the model divertor tokamak equilibrium and the corresponding ballooning mode equation introduced in Ref. [6]. The detailed construction of the model and the derivation of the ballooning equation are given in Ref. [9].

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Using a technique devised by Mercier and Luc [10] the Grad-Shafranov equation is solved locally by expansion in the neighbourhood of a single flux surface. The equilibrium is determined once the shape of the surface and the poloidal magnetic field on the surface have been specified. This information is taken from the magnetic field structure surrounding a pair of long and thin parallel wires carrying equal currents [11]. This linear vacuum system is used only to generate a single magnetic surface; the equilibrium itself is calculated in toroidal geometry at finite beta. The shape of the magnetic surface is specified in polar co-ordinates \((r, \theta)\) by the implicit relation

\[
k^2 = \frac{r^2}{r_0^2} \left[ \frac{1}{\sqrt{1+k}} - 1 \right]^2 \left[ 4 + \frac{r^2}{r_0^2} \left( \frac{1}{\sqrt{1+k}} - 1 \right)^2 - 4 \frac{r}{r_0} \cos(\theta - \gamma) \left( \frac{1}{\sqrt{1+k}} - 1 \right) \right]
\]

(1)

\(r(\theta) = r_0 g(\theta)\)

where \(k\) is a parameter controlling the shape of the surface such that as \(k \to 0\) the surface becomes a circle and as \(k \to 1\) the shape of the surface approaches that of a separatrix. Equation (1) is normalized so that the value of \(r\) opposite the X-point is held fixed \((r = r_0)\), independent of \(k\). Examples of surfaces with different values of \(k\) are shown in Fig. 1. This diagram also defines the angle \(\gamma\) which controls the poloidal location of the X-point.

The corresponding poloidal magnetic field on the flux surface is given by

\[
\left[ \frac{B_p(\theta)}{B_{p0}} \right] = \left[ 1 + \frac{r^2}{r_0^2} \left( \frac{1}{\sqrt{1+k}} - 1 \right)^2 \right] - \frac{2r}{r_0} \left( \frac{1}{\sqrt{1+k}} - 1 \right) \cos(\theta - \gamma) \right] \left( \frac{1}{1+k} \right)
\]

\[
= [b(\theta)]^2
\]

(2)

in which the value of the poloidal field opposite the X-point is held fixed at \(B_p = B_{p0}\) independent of \(k\).

Throughout this paper we consider a large aspect ratio tokamak. We therefore write the major radius \(X(\theta)\) at a point on the flux surface in the form

\[
X(\theta) = X_0 + \delta X(\theta)
\]

for which \(X_0\) is defined in Fig. 1. We then take the high-beta tokamak ordering

\[
\frac{\delta X}{X_0} \sim \frac{r_0}{X_0} \sim \frac{p}{B_0} \sim \frac{B_p}{B} \sim \varepsilon
\]

(where \(p\) is the plasma pressure and \(B\) is the total magnetic field) and keep only the leading order contributions in a small-\(\varepsilon\) expansion.

The ballooning equation in large aspect ratio corresponding to this equilibrium can be written

\[
\frac{b}{h} \frac{d}{d\theta} \left[ \frac{1}{b^2 + P^2(\theta)} \right] \frac{b}{h} \frac{dF}{d\theta} = \frac{\varepsilon}{b} \sin u + \cos u \ F(\theta) = 0
\]

(3)

Here we have written the poloidal arclength as \(dl = r_0 h(\theta) d\theta\), with

\[
h(\theta) = \left[ g^2 + (g')^2 \right]^{1/2}
\]

The function \(P(\theta)\) is defined by

\[
P(\theta) = b \int_{\delta_0}^{\theta} \frac{hd\theta}{b^3} \left[ \frac{\alpha + \frac{2b}{r} - \frac{\delta X}{r_0}}{r_0} \right]
\]

and \(u\) is the angle between the local tangent to the flux surface and the X-direction. Also, \(f(\theta) = R(\theta)/r_0\), where \(R(\theta)\) is the Gaussian radius of curvature of the flux surface given by
\[ R(\theta) = \frac{[r^2 + (r')^2]^{3/2}}{[r^2 + 2(r')^2 - r r'']} \]

Finally we have introduced the parameters

\[ \sigma = \left( p' + \frac{I'^{I'}}{X_0} \right) \frac{X_0 r_0}{B_{p0}} \]

\[ \alpha = -2p' r^2 \frac{j}{B_{p0}} \]

(4)

(5)

where \( I(\psi) \) is the toroidal field function

\[ \hat{B} = \frac{1}{X_0} \hat{\vec{e}}_\theta + \nabla \psi \times \nabla \phi, \]

\( \phi \) is the toroidal angle, and primes denote derivatives with respect to the poloidal flux \( \psi \). Note that the pressure gradient parameter \( \alpha \) defined here reduces to the \( s-\alpha \) definition \([5]\) when \( k \to 0 \). As a consequence of the ballooning transformation \([12]\) the poloidal angle \( \theta \) in Eq. (3) lies on \([-\infty, \infty] \). Equation (3) is solved with the boundary conditions \( F(\pm \infty) = 0 \) and can be regarded as an eigenvalue equation for \( \alpha \).

In Section 4 we shall be interested in studying the dependence of the stability properties on the toroidal current density. Although \( \sigma \) is closely related with the current density, its value depends on the (arbitrary) definition of \( X_0 \); that is if we transform

\[ X_0 \to X_0 + C, \quad \delta X \to \delta X - C \]

(6)

where \( C/X_0 = \) constant \( \epsilon \), then \( \sigma \) is not invariant at leading order in \( \epsilon \). This follows from the partial cancellation of \( \frac{p'}{p'} \) and \( \frac{I'^{I'}}{I'^{I'}} \):

\( \frac{p'}{p'} + \frac{I'^{I'}}{I'^{I'}} \frac{X_0}{X_0} \frac{r_0}{r_0} = 0(\epsilon) \)

Thus, using Eq. (6), we have

\[ p' + \frac{I'^{I'}}{X_0} \to p' + \frac{I'^{I'}}{X_0} - 2 \frac{C}{X_0} \frac{I'^{I'}}{X_0} \]

and the extra term must be retained at leading order. Instead of using \( \sigma \), we proceed as follows. From Ohm’s law we can write

\[ \eta \int \hat{J} \cdot \hat{B} = -\hat{B} \cdot \nabla \Phi + \hat{B} \cdot \hat{E}^A \]

where \( \hat{E}^A \) is the inductive contribution to the electric field, \( \eta \) is the resistivity and \( \Phi \) is the electrostatic potential. We can annihilate \( \hat{B} \cdot \nabla \Phi \) by integration round the flux surface (since \( \Phi \) must be single-valued):

\[ \int \frac{dl}{B_p} \hat{B} \cdot \nabla \Phi = 0 \]

Writing \( \hat{E}^A = E^A \hat{\vec{e}}_\theta \), where \( E^A = V/2\pi X \) and \( V \) is the loop voltage, and using \( \hat{J} \cdot \hat{B} = J || B = -I'B^2 - Ip' \), we have

\[ \int \frac{dl}{B_p} (I'B^2 + Ip') = \int \frac{dl}{B_p} \frac{B \Phi V}{2\pi X} \]

(7)

It is convenient at this point to introduce a number of surface-averaged quantities which are defined as follows:

\[ W = \frac{1}{2\pi} \int \frac{h \theta}{b} \frac{\delta X}{r_0} \]

\[ A = \frac{1}{2\pi} \int \frac{h \theta}{b^3} \]

\[ D = \frac{1}{2\pi} \int \frac{h \theta}{b} \]

\[ H = \frac{1}{2\pi} \int \frac{h \theta}{f b^2} \frac{\delta X}{r_0} \]

\[ G = \frac{1}{2\pi} \int \frac{h \theta}{b^3} \frac{\delta X}{r_0} \]

\[ F = \frac{1}{2\pi} \int \frac{h \theta}{f b^2} \]

\[ T = \frac{1}{2\pi} \int \frac{h \theta}{b^2} \sin u \]

(8)

We now expand Eq. (7) in large aspect ratio, taking account of the partial cancellation in \( p' + I'^{I'}/X_0 \) and keeping the leading order contribution. This gives

\[ \Lambda = \frac{\alpha}{D} - \sigma \]

(9)

where \( \Lambda \) is defined by

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\[ \Lambda = \left( \frac{r_0 V}{2\pi X_0 B_{\phi p0} \eta} \right) \]  

(10)

Note that Eq. (9) is invariant under Eq. (6).

We are interested in solving the ballooning equation on flux surfaces near the edge of the plasma. Since these will be relatively cool and therefore resistive, we begin by setting the toroidal current density parameter \( \Lambda \) to zero and using Eq. (9) to eliminate \( \sigma \) in Eq. (3). This treatment of the edge region avoids the dependence on the arbitrary quantity \( X_0 \) which occurs if \( \sigma \) is set to zero as was done in Ref. [6]. As a result, the solutions of the ballooning equation as compared with those of Ref. [6] are somewhat modified.

Figure 2 shows a plot of \( \alpha \) against \( k \) for \( \gamma = \pi/2 \), corresponding to the (single null) divertor configurations in ASDEX and DOUBLET III. These show two stable regions separated by a region unstable to ballooning modes. Figures 3 and 4 show the corresponding plots for \( \gamma = 3\pi/4 \), corresponding to the PDX configuration, and \( \gamma = \pi \), in which the X-point is on the inside of the torus. Note that the first stability boundary is essentially independent of \( \gamma \) while the second boundary shows a strong dependence on \( \gamma \), with the unstable region shrinking as the X-point is moved further round to the inside of the torus. We can define the global shear parameter \( s \) by [6]

\[ s = \frac{X_0r_0B_{\phi p0}}{q} \frac{dq}{d\psi} \]  

(11)

which reduces to the \( s-\alpha \) definition when \( k \to 0 \). An expression for \( s \) is derived in Ref. [9] and can be written

\[ s = \frac{\sigma \Lambda + 2F - \alpha G}{D} \]  

(12)

Figure 5 is a plot of \( s \) against \( k \) for values of \( \alpha \) corresponding to the first stability boundary of Fig. 3. (Again we eliminate \( \sigma \) in favour of \( \Lambda \), and set \( \Lambda = 0 \).)
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where the various flux surface integrals are as defined in Eq. (8).

The limit $k \to 0$ represents the large aspect ratio tokamak with $B_p(0) = \text{constant}$. This is the $s$-$\alpha$ model introduced in Ref. [5]. To see its connection with the present study, we eliminate $\sigma$ in favour of the global shear $s$ given by Eq. (12). Note that $s$ is invariant under Eq. (6). Using Eq. (12) to eliminate $\sigma$ in Eq. (14), the marginal stability condition $D_M = 0$ becomes

$$s^2 = \frac{4(2AH - AT - 2FG)}{D^2}$$  

(15)

In the limit $k \to 0$ we obtain $s^2 = 0$, showing that interchange modes are irrelevant for the $s$-$\alpha$ model.

As we did for ballooning modes, we eliminate $\sigma$ in Eq. (14) in favour of $\Lambda$ as defined by Eq. (9). The criterion for marginal stability, $D_M = 0$, can then be written

$$(G - WA/D)^2 \left[ \frac{\alpha^2}{2} \right]$$

$$- (4AH - 2AT - 2FG - 2WAF/D - \Lambda AG + \Lambda WA^2/D)$$

$$\times \left[ \frac{\alpha}{2} \right] + (F - \Lambda A/2)^2 = 0$$  

(16)

By numerical evaluation of the various loop integrals in Eq. (16) we can solve for the marginally stable $\alpha$ in terms of the parameters $\gamma$, $k$ and $\Lambda$.

**3. STABILITY OF IDEAL INTERCHANGE MODES**

The criterion derived by Mercier [13] states that ideal interchange modes will be unstable if $D_M < 0$, with $D_M$ defined as follows:

$$D_M = \frac{1}{4} - \frac{p'}{(2\pi q')^2} \left( \frac{\partial}{\partial \psi} \int \frac{dl}{B_p} - p' \int \frac{dl}{B_p^3} \right) \int \frac{B^2 dl}{X^2 B_p^3}$$

$$+ \int \left( I^2 \frac{p'}{(2\pi q')^2} \right) \int \frac{dl}{X^2 B_p^3}$$

(13)

Here, $q(\psi)$ is the safety factor and $q'$ is evaluated in Ref. [9]. Expanding in large aspect ratio and keeping the leading order contribution, we obtain

$$D_M = \frac{1}{4} - \frac{\alpha(2AH - 2FG - AT)}{(\alpha A + 2F - \alpha G)^2}$$

(14)

**FIG. 5. Global shear $s$ as a function of $k$, along the first stability boundary of Fig. 3.**

We see that $s \to \infty$ as $k \to 1$, even though $\alpha$ remains finite. This is in marked contrast to the $s$-$\alpha$ model, in which large shear implies a large value of the marginally stable $\alpha$.

Consideration of cases with $0 \leq \gamma \leq \pi/2$ must be postponed until we have studied the effects of interchange modes in the next section.

**FIG. 6. Marginally stable $\alpha$ for interchange modes as a function of $k$ for $\gamma = 0$, $\Lambda = 0$. First ballooning boundary shown by broken line.**
For $\gamma < \pi/2$ (and $\Lambda > 0$), Eq. (16) has two positive roots which define the boundaries of the first and second stable regions. As $\gamma \to \pi/2$, $\alpha \to \infty$, and for $\gamma > \pi/2$ the roots for $\alpha$ are negative. Thus for normal tokamak pressure profiles the interchange mode will always be stable whenever $\gamma > \pi/2$. For this reason it was not necessary to consider interchange modes in plotting Figs 2, 3 and 4.

Again we begin by considering $\Lambda = 0$ and in Fig. 6 we plot $\alpha$ against $k$ for $\gamma = 0$, corresponding to the divertor configuration in JT-60. This figure also shows the corresponding first ballooning stability boundary obtained by solving Eq. (3) with $\Lambda = 0$.

In Fig. 6 the ballooning boundary has only been plotted as far as the interchange mode threshold. Beyond this, the numerical solution of the ballooning equation is no longer meaningful and the stability boundary is determined by the interchange mode. This follows from the relation between ballooning and interchange modes discussed in Ref. [12]. Asymptotically the solution to the ballooning equation, Eq. (3), behaves like

$$F(\theta) \sim F_1 \theta^{\lambda_1} + F_2 \theta^{\lambda_2}$$

where the two values of $\lambda$ are

$$\lambda_1 = -\frac{1}{2} - \sqrt{D_M}, \quad \lambda_2 = -\frac{1}{2} + \sqrt{D_M}$$

For $D_M > 0$, only the small solution is acceptable since the large solution (even though it tends to zero if $D_M \leq \frac{1}{4}$) leads to a divergent energy functional $5W$. Numerically we distinguish these two solutions by solving the ballooning equation on a finite interval ($-\theta_{\text{max}} \leq \theta \leq \theta_{\text{max}}$) and imposing the boundary condition $F(\pm \theta_{\text{max}}) = 0$. This has the effect of setting

$$\frac{F_2}{F_1} = \frac{\theta_{\text{max}}}{\lambda_1 - \lambda_2}$$

Then, provided $\theta_{\text{max}}$ is sufficiently large, we have $F_2/F_1 \to 0$ and we pick out only the small solution. (In practice we ensure that $\theta_{\text{max}}$ is large enough by checking that the eigenvalue is insensitive to the value of $\theta_{\text{max}}$.) However, as we approach the Mercier stability boundary $D_M = 0$, we have $(\lambda_1 - \lambda_2) \to 0$ and we need to use ever larger values of $\theta_{\text{max}}$ to pick out the small solution until we exceed some numerical limitation. In the interchange unstable region, both solutions are oscillatory and the numerical method breaks down completely. Although eigenvalues can still be found, they can be distinguished from genuine solutions by their sensitivity to the value of $\theta_{\text{max}}$.

4. EFFECTS OF FINITE CURRENT DENSITY

In this section we investigate the effects of non-zero values of the current density parameter $\Lambda$. We begin by considering $\gamma = 3\pi/4$, with $k = 0.95$. From the previous section it follows that we do not need to consider interchange modes since the X-point is on the inside of the torus. Therefore, in Fig. 7 we plot $\alpha$ against $\Lambda$ for the first and second marginally stable ballooning boundaries. We see that for $\Lambda > 0.7$ the first and second regions have coalesced and there is no longer an instability to ballooning modes. In Fig. 8 we plot $\alpha$ against $k$ for $\gamma = 3\pi/4$ and $\Lambda = 0.8$. We see that for surfaces sufficiently close to the separatrix ($k \geq 0.9$) there is no ballooning unstable region and hence no ballooning limit to the pressure gradient.

For $\gamma < \pi/2$ we again have to consider interchange modes. In Fig. 9 we plot $\alpha$ against $\Lambda$ for $\gamma = 0$ and $k = 0.95$. Again we see that the first and second stable regions coalesce. However, the first stability boundary now extends down to $\alpha = 0$. The reason for this is easily seen by differentiating Eq. (16) with respect to $\Lambda$ at fixed $k$ and $\gamma$. There will be a minimum in $\alpha$ at

![Figure 7](image)

**Fig. 7.** Marginally stable $\alpha$ as a function of $\Lambda$ for $\gamma = 3\pi/4$ and $k = 0.95$, showing coalescence of the first and second stable regions.
5. INTERPRETATION OF THE ABSENCE OF BALLOONING INSTABILITIES

A simple explanation for the absence of ballooning instabilities on flux surfaces sufficiently close to the separatrix can be given on the basis of ideas introduced in Ref. [14]. This process is very similar to the mechanism which stabilizes the ballooning mode in a strongly indented bean-shaped plasma [15]. We begin by considering the local shear $S$ defined by

$$ S = \frac{\mathbf{B} \times \nabla \psi}{|\nabla \psi|^2} \cdot \nabla \times \left( \frac{\mathbf{B} \times \nabla \psi}{|\nabla \psi|^2} \right) $$

Ballooning modes tend to be localized along the field line in regions where the local shear is small or zero. In equilibrium an increased pressure gradient is balanced by a strengthening of the poloidal field on the outside of the torus and this decreases the local shear and can reverse its sign. A further increase of the pressure gradient causes the points of zero local shear to move round the surface away from the region of destabilizing curvature. The ballooning instability is usually encountered well before these points reach the good curvature region on the inside of the torus. However, if the equilibrium can be modified (in this case by the introduction of non-zero $\Lambda$) in such a way that the zeros of local shear always lie in the good curvature region then, as shown in Ref. [14], the

$\Lambda = 2F/A$ and the minimum value will be $\alpha = 0$. Since the removal of the unstable region requires a minimum in $\alpha$, a point where $\alpha = 0$ will necessarily be present. In Fig. 10 we plot $\alpha$ against $k$ for $\gamma = 0$ and $\Lambda = 0.8$. (The first ballooning boundary is also shown.) Again we see the coalescence of the stability boundaries and the existence of a point where the marginal $\alpha$ vanishes.
ballooning mode will always be stable. This provides a simple interpretation for the results of the previous section and leads to a rough estimate for the boundary of the ballooning unstable region.

Expanding Eq. (17) in large aspect ratio we obtain

$$S = \frac{N}{b^2(\theta)} \left[ \alpha \frac{W}{D} - \alpha \frac{\delta X}{r_0} - \alpha \frac{2b(\theta)}{f(\theta)} \right]$$ (18)

where $N = 1/(X_{\theta}^{\alpha} r_0 B_{\theta})$. The normalized surface average of Eq. (18) gives the global shear, Eq. (12).

We also need to find the angle $\theta_k$ at which the normal curvature changes sign. This occurs when

$$K \propto \frac{1}{B^2} \frac{\partial^2}{\partial \psi^2} (p + \frac{1}{2} B^2) = 0$$

which in large aspect ratio reduces to $\partial X/\partial \psi = 0$. From Ref. [9] this is equivalent to $\sin \theta_k = 0$. Again we consider $\gamma = 3\pi/4$ and $k = 0.95$. Since the flux surface is not up-down symmetric, there will be two values of $\theta$ at which $K$ vanishes, these being $\theta_k = 0.635\pi$ and $\theta_k = -0.535\pi$. In Fig. 11 we show the ballooning unstable region on an $\alpha$-$\Lambda$ diagram (this is Fig. 7 replotted on a smaller scale). Also shown are the lines along which $S = 0$ at $\theta = \theta_k$ obtained by evaluating Eq. (18). In the region to the right of these lines the zeros of local shear always occur in the favourable curvature region and so any ballooning instabilities must be confined to the remainder of the $\alpha$-$\Lambda$ diagram. This is indeed seen to be the case and supports the interpretation given above for the coalescence of the first and second stable regions.

6. A PICTURE OF THE H-MODE

The results of Section 4 lead us to suggest the following simple picture of L- and H-mode regimes in divertor tokamaks. In the L-mode the edge temperature and hence the current density are relatively low and the stability diagram has the form shown in Fig. 3. The edge pressure gradient is then ballooning limited. If the edge temperature can be raised (for instance by the passage of a heat pulse from a sawtooth instability) then the corresponding increased current density can lead to a stability diagram like Fig. 7. The edge pressure gradient can now become very steep. This corresponds to an increased temperature just inside the separatrix. The resulting increased current density maintains the form of the stability diagram and leads to the bistable nature of the L-H transition. Further into the plasma the pressure gradient is again ballooning limited.

Using the value $\Lambda = 0.7$ from Fig. 6, together with the definition of $\Lambda$ (Eq. (10)) and the Spitzer resistivity formula, we obtain $T_{edge} \approx 350$ eV, in broad agreement with the observed values. Also, using data from PDX published in Ref. [3], we can compare the calculated stability diagrams with experimental values of $\alpha$ (see Fig. 6 of Ref. [3]). For the L-mode we obtain $\alpha \approx 0.36$ which fits well with the first stability boundary of Fig. 3. Similarly for the H-mode we obtain $\alpha \approx 3.6$ for the very steep profiles close to the separatrix. Comparison with Fig. 7 shows that this value lies well into the second region of stability which is accessible because of the absence of the ballooning unstable region near the plasma edge. Further in from the separatrix the experimental H-mode profiles are less steep and give $\alpha \approx 0.52$, which can again be compared with Fig. 7 and which is consistent with the end of the ballooning unstable zone at $k \approx 0.9$.

With the X-point on the outside of the torus we see that whenever the first and second stable regions coalesce there is a flux surface on which $\alpha = 0$. This may have a bearing on the prospects for achieving H-mode operation in JT-60 and could adversely affect the pressure profiles which might be obtained.
7. CONCLUSIONS

We have investigated the stability of a model divertor tokamak equilibrium to ideal ballooning modes and to ideal and resistive interchange modes. This work may also be of interest in connection with conventional tokamaks when a magnetic separatrix is introduced into the vacuum vessel, as has been proposed for JET [16]. Comparison of the stability diagrams for various values of $\gamma$ (the poloidal location of the X-point) supports the conclusion, reached in Ref. [6], that the stability properties become progressively better as the X-point is moved round to the inside of the torus. Inclusion of finite current density shows the possibility of achieving complete stability to ballooning and interchange modes for surfaces sufficiently close to the separatrix. This lead to a picture of the H-mode in which the absence of ballooning instability permits the very large edge pressure gradient.

Appendix

RESISTIVE INTERCHANGE MODES

The effect on interchange modes of allowing finite resistivity and consequent field line reconnection is to modify the Mercier criterion (13) to read [17]

$$D_R < 0$$  \hspace{1cm} (A1)

where

$$D_R = D_M - \left[ \frac{1}{4} - H \right]^2$$

$$H = \frac{\int_0^1 B^2 \, dl}{(2\pi)(2\pi)} \left\{ \frac{\int B^2 \, dl}{B_p} - \frac{\int B^2 \, dl}{B_p} \right\}
\left\{ \frac{\int B^2 \, dl}{B_p} + \frac{\int B^2 \, dl}{B_p} \right\}
\left\{ \frac{\int B^2 \, dl}{B_p} - \frac{\int B^2 \, dl}{B_p} \right\}
\left\{ \frac{\int B^2 \, dl}{B_p} + \frac{\int B^2 \, dl}{B_p} \right\}
\left\{ \frac{\int B^2 \, dl}{B_p} - \frac{\int B^2 \, dl}{B_p} \right\}
\left\{ \frac{\int B^2 \, dl}{B_p} + \frac{\int B^2 \, dl}{B_p} \right\}$$

Again we expand in powers of the inverse aspect ratio and keep the leading order contribution. This yields

$$H = \frac{\alpha G - W\Lambda/D}{(\alpha A + 2F - \alpha G)}$$  \hspace{1cm} (A2)

for which the various loop integrals are defined by Eq. (8). (At this order there are no cancellations between $H$ and $D_M$ to consider.) Using Eq. (14) for $D_M$ we have

$$D_R = \frac{\alpha A \left[ T - 2H + 2WF/D + \Lambda G - \Lambda W A/D \right]}{(\alpha W A/D - \Lambda A + 2F - \alpha G)^2}$$  \hspace{1cm} (A3)

where again we have eliminated $\sigma$ in favour of $\Lambda$ using Eq. (9). Note that for $\alpha > 0$ the sign of $D_R$ is independent of the value of $\alpha$ and depends only on $\gamma$, $k$, and $\Lambda$. By inspection of Eq. (A3) we see that for $\Lambda = 0$ we have $D_R < 0$ if $\gamma < \pi/2$ and we have $D_R > 0$ if $\gamma > \pi/2$, so that the resistive interchange mode will be unstable if the X-point is located on the outside of the torus. For non-zero $\Lambda$ the sign of $D_R$ can be changed and the mode stabilized.

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